



# ME 327: Design and Control of Haptic Systems

## Spring 2020

# Lecture 8:

# Kinesthetic haptic devices: sensors and actuators

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# sensors

# sensing systems

- magnetic



magnetic: TrakStar, Ascension

- optical



optical: Polaris, NDI

- acoustic



optical: Microsoft Kinect



acoustic: ultrasonic proximity sensor, BiF



inertial: wearable IMU, MotionNode

- inertial

- **mechanical**

(our focus, since these are the sensors typically integrated with the actuator in kinesthetic haptic devices)

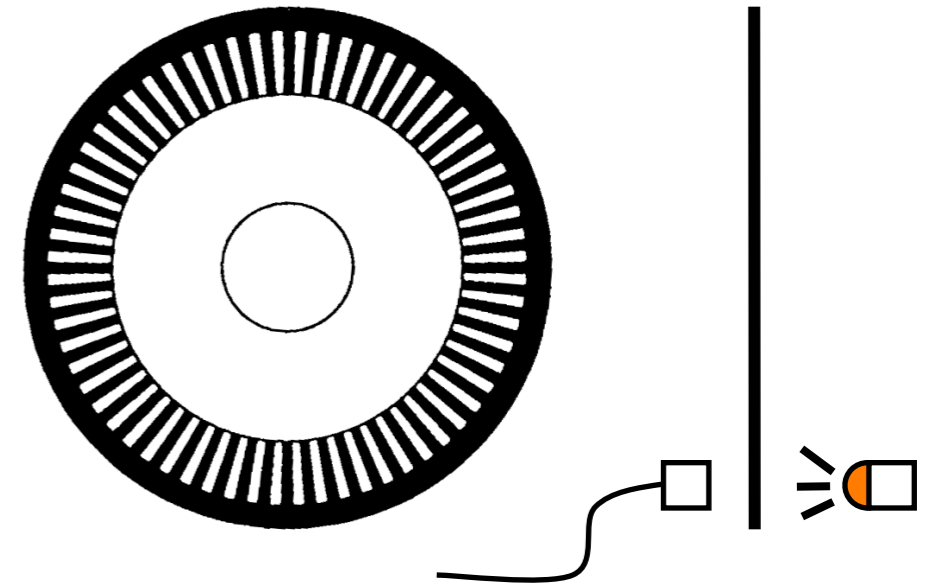


mechanical: Faro arm

# mechanical trackers

- ground-based linkages most commonly used
- joint position sensors
  - digital: optical encoders are most common
  - analog: magnetic sensors and potentiometers are most common

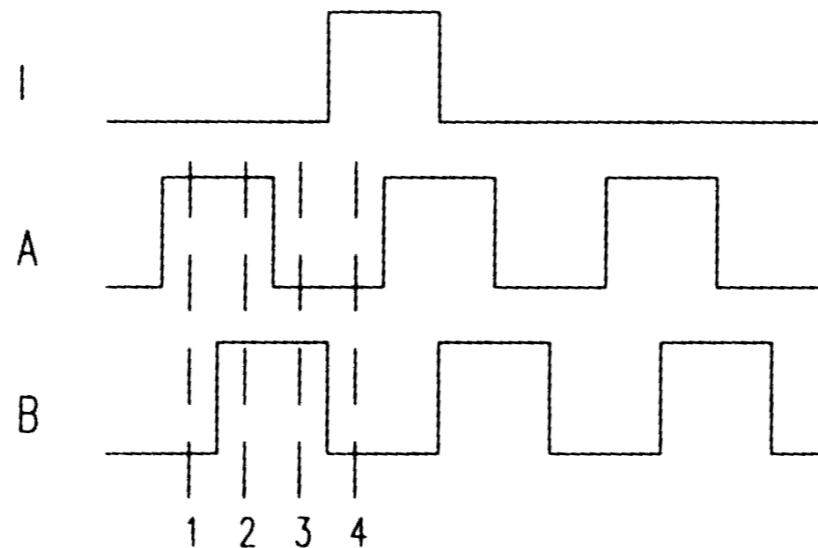
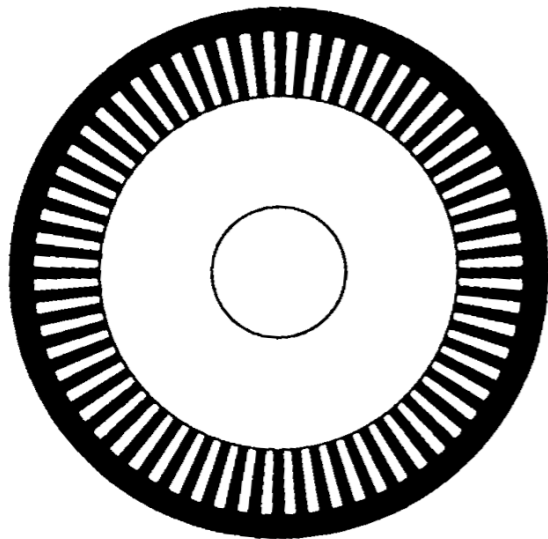
# optical encoders



- how do they work?
  - A focused beam of light aimed at a matched photodetector is interrupted periodically by a coded pattern on a disk
  - Produces a number of pulses per revolution (Lots of pulses = high cost)
- quantization problems at low speeds
- absolute vs. referential

# optical encoders

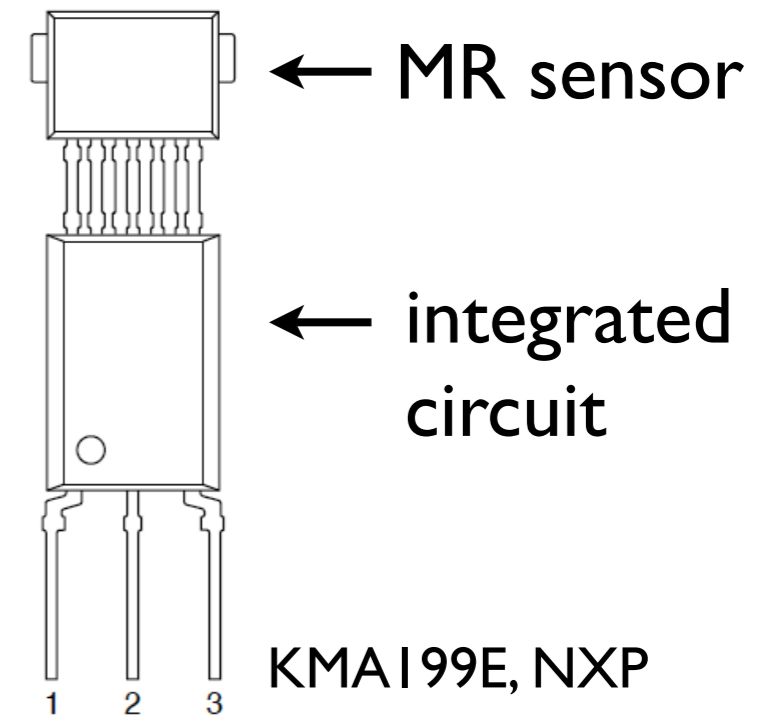
- phase-quadrature encoder



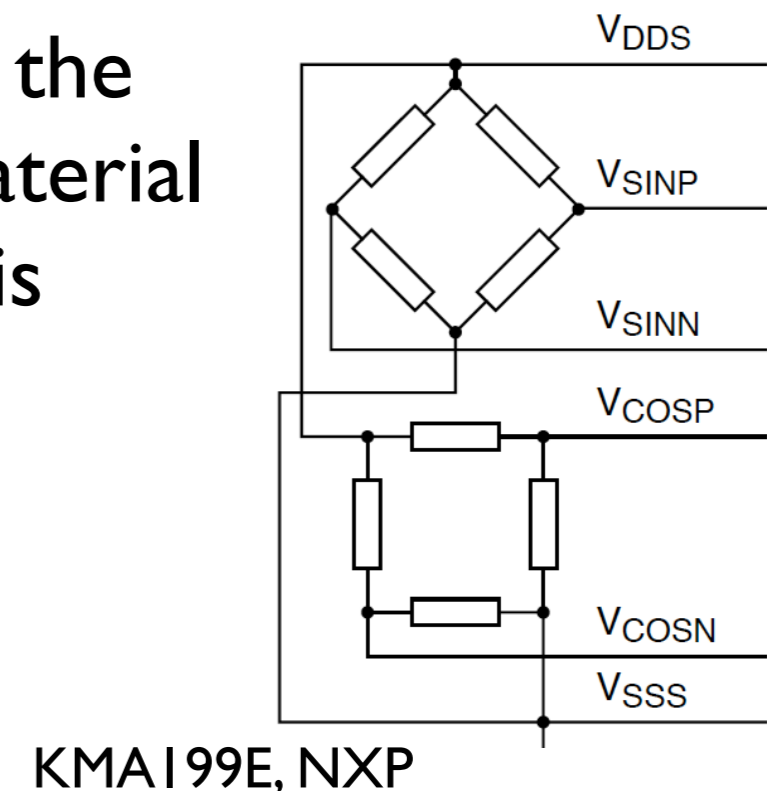
State	Ch A	Ch B
S1	High	Low
S2	High	High
S3	Low	High
S4	Low	Low

- 2 channels,  $90^\circ$  out of phase
  - allows sensing of direction of rotation
  - 4-fold increase in resolution

# magneto-resistive angle sensors

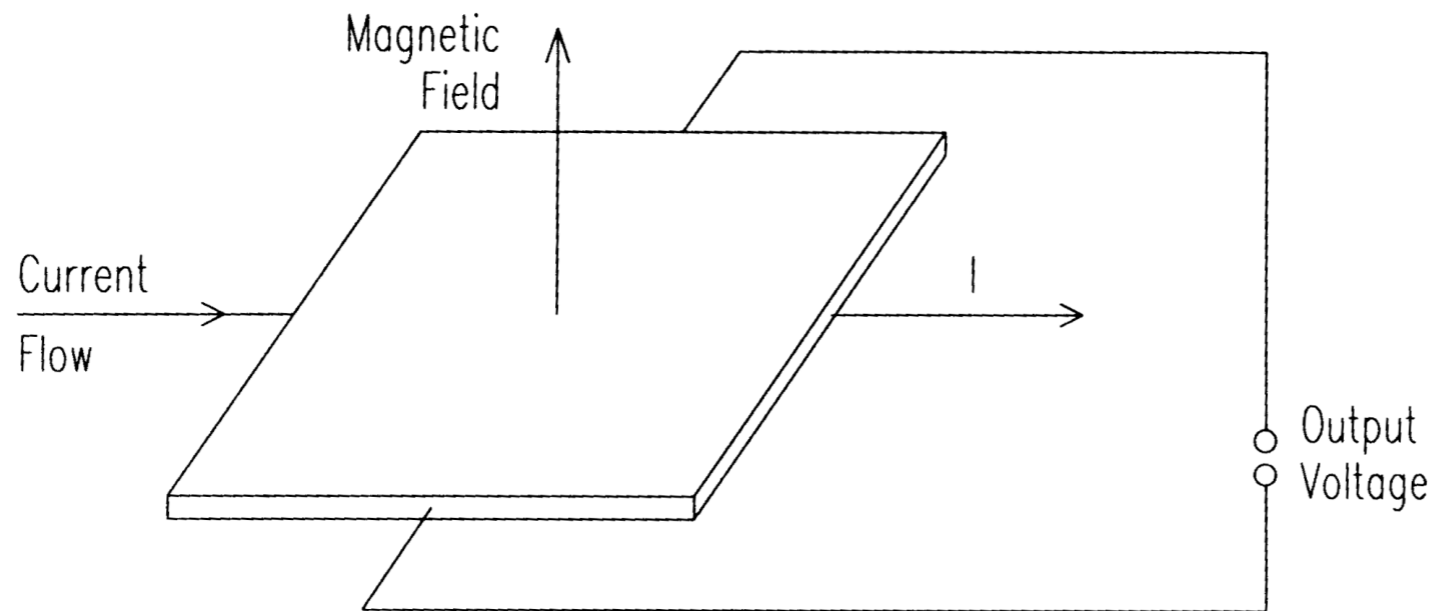


- magneto-resistive materials change their electrical resistance when an external magnetic field is applied
- the resistance depends on the angle between the magnetization vector of the ferromagnetic material and the direction of current flow (resistance is largest if they are parallel)
- often 4 sensors are connected in a Wheatstone bridge configuration (similar to strain gages)



# Hall-Effect Sensors

a small transverse voltage is generated across a current-carrying conductor in the presence of a magnetic field



(Discovery made in 1879, but not useful until the advent of semiconductor technology.)



# Hall-Effect Sensors

$$V_h = \frac{R_h IB}{t}$$

$V_h$  = Hall voltage

$R_h$  = Hall coefficient

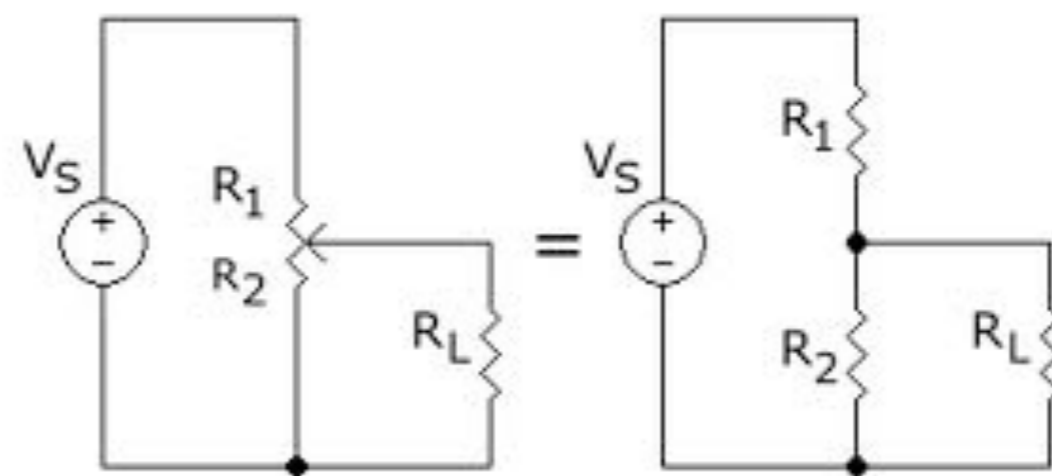
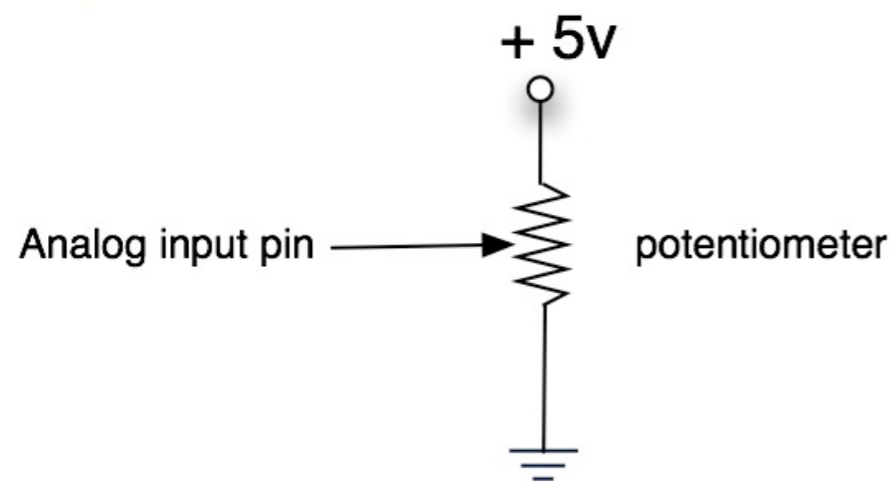
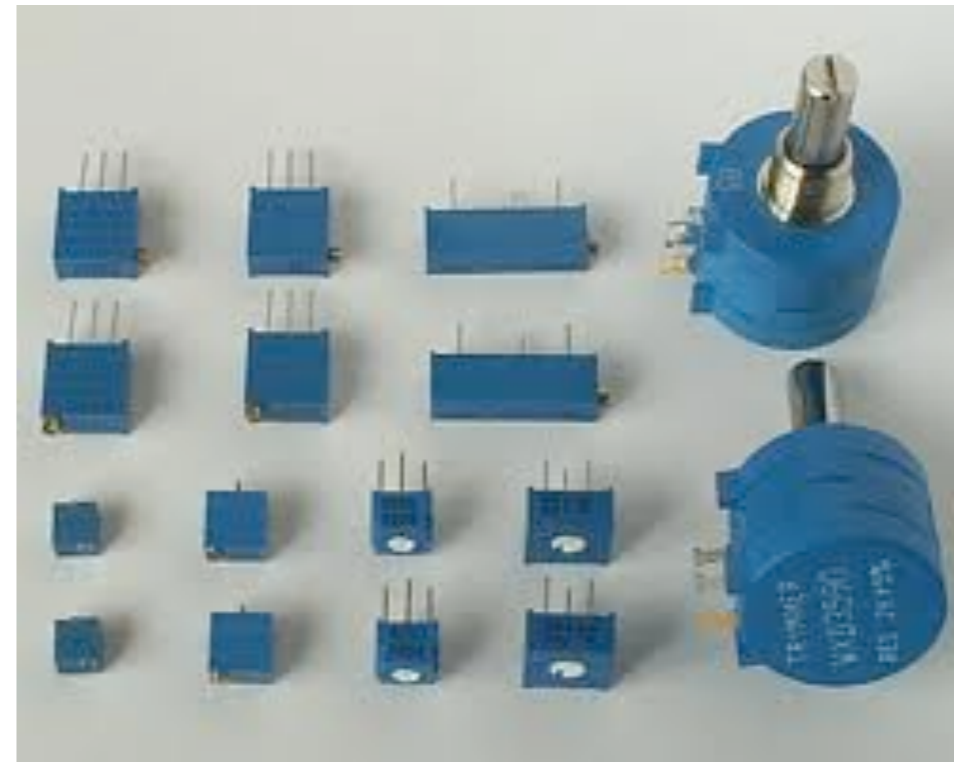
$I$  = Current

$B$  = Magnetic flux density

$t$  = Element thickness

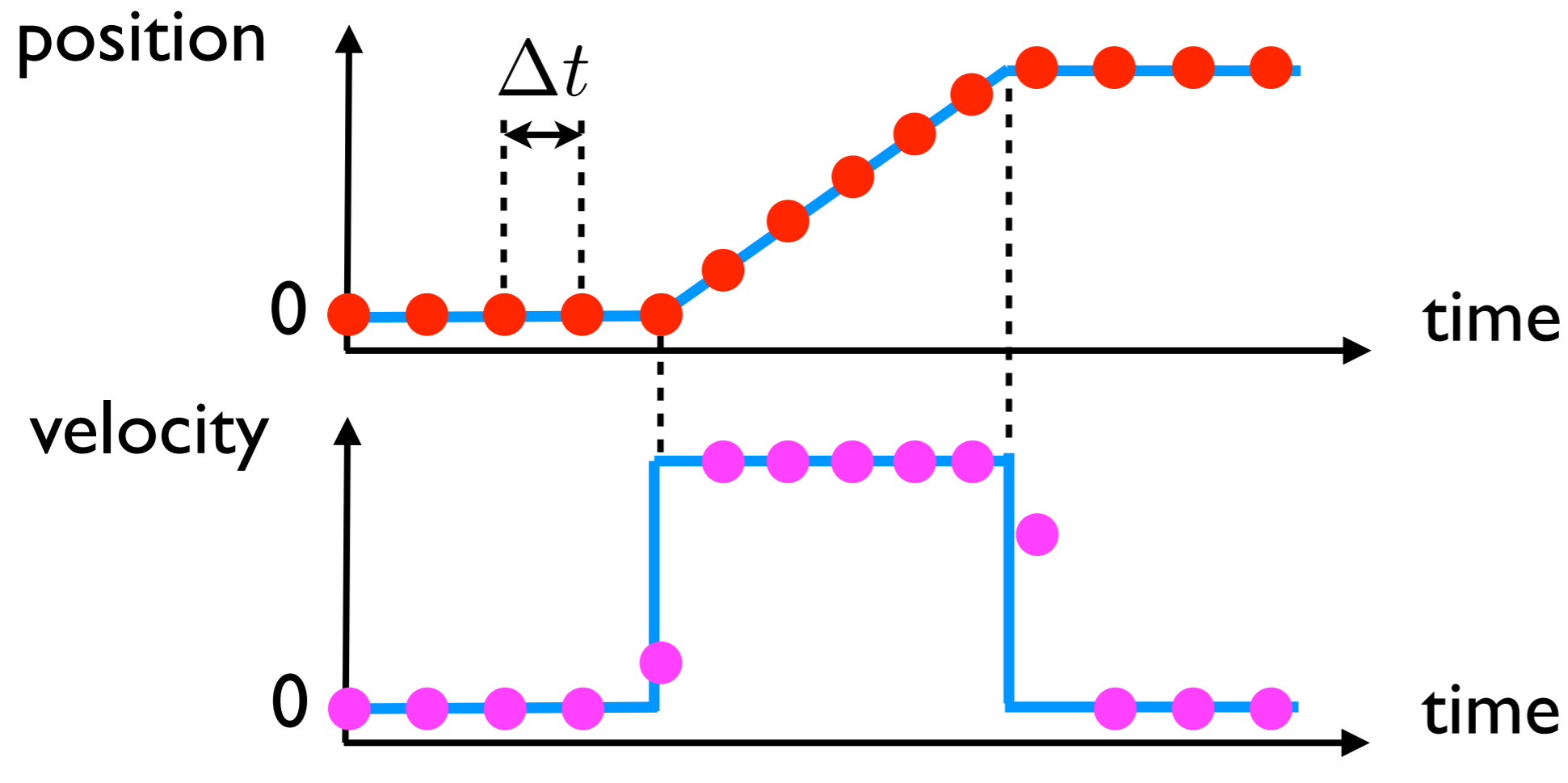
- amount of voltage output related to the strength of magnetic field passing through.
- linear over small range of motion (need to be calibrated)
- affected by temperature, other magnetic objects in the environments

# potentiometers



# position, velocity, and acceleration

For the Hapkit, you can access position and time data from your Hapkit board



$$v_{\text{inst}} = \frac{dx}{dt} = \dot{x}$$

$$v_{\text{avg}} = \frac{\Delta x}{\Delta t}$$

acceleration is usually too noisy

# measuring velocity

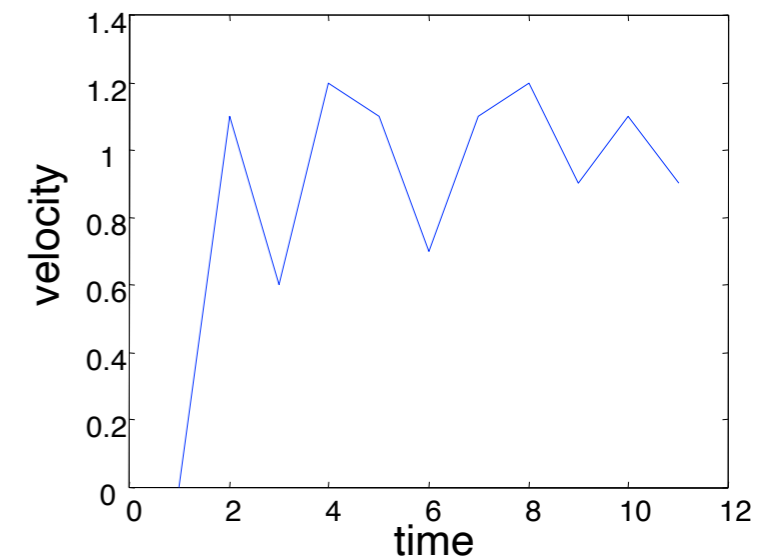
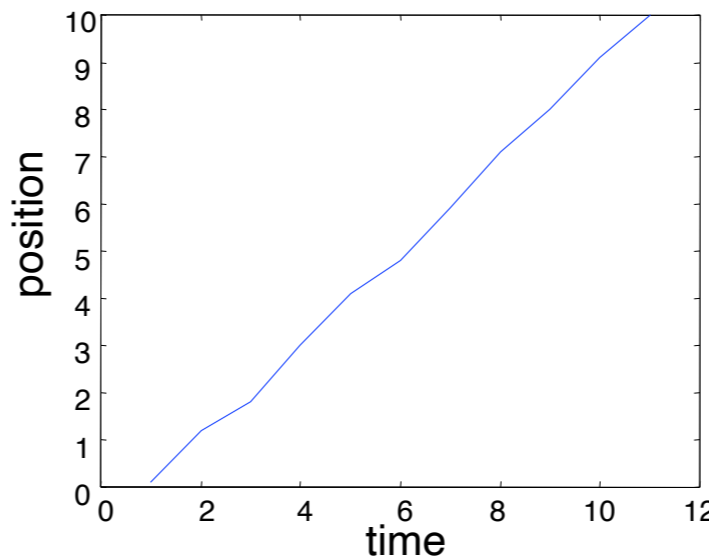
- differentiate position
  - advantage: use same sensor as position sensor
  - disadvantage: get noisy signal
- alternative
  - for encoders, measure time between ticks

# discrete differentiation

- many different methods
- simple example:
  - average 20 readings = P1
  - average next 20 readings = P2
  - where t is the the period of the servo loop

$$V = \frac{P1 - P2}{t}$$

- differentiation increases noise
- usually need to filter



# position/velocity filtering

- one example is the simple infinite impulse response (IIR) filter

```
// Return RC low-pass filter output samples, given input samples,  
// time interval dt, and time constant RC  
function lowpass(real[0..n] x, real dt, real RC)  
  var real[0..n] y  
  var real  $\alpha$  := dt / (RC + dt)  
  y[0] := x[0]  
  for i from 1 to n  
    y[i] :=  $\alpha$  * x[i] + (1- $\alpha$ ) * y[i-1]  
  return y
```

- pseudocode for real-time filtering:  
new\_value = read\_from\_sensor()  
filtered\_value =  $a$ \*new\_value + (1- $a$ )\*old\_value  
old\_value = filtered\_value

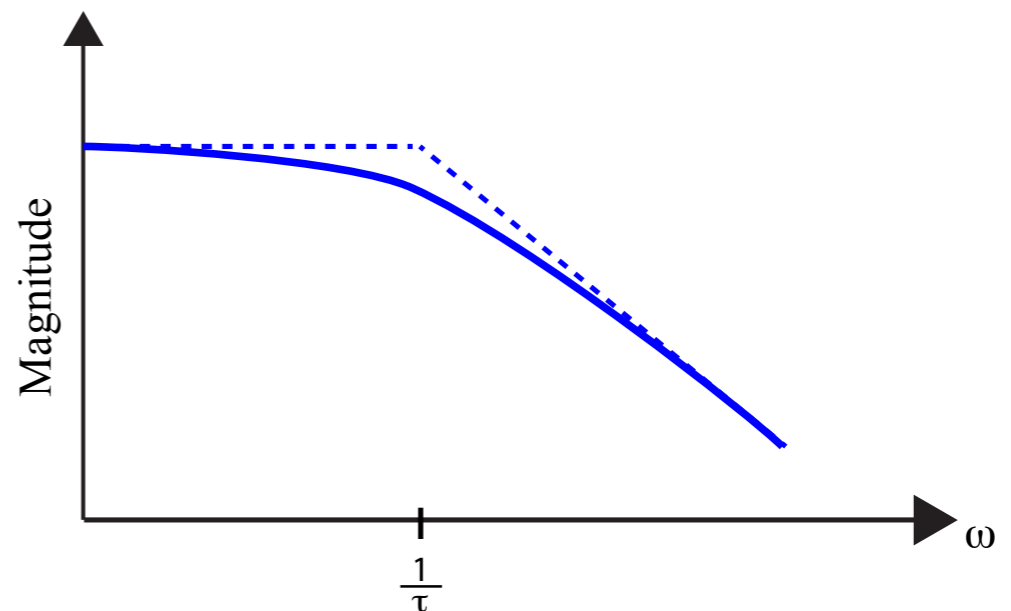
# IIR filter

single-pole infinite impulse response (IIR) low-pass filter,  
also called an exponential moving average filter

$$H = \frac{1}{\tau s + 1}$$

$\tau$  is defined as one divided by the cutoff frequency, i.e.  $\tau = \frac{1}{\omega_c}$

You choose the cutoff frequency to be the frequency at which the amplitude of the response begins to roll off.



# IIR filter

implementing in the (discrete) time domain:  
compute a weighting parameter  $\alpha$  that determines the relative weight of old versus new measurements.

$$\alpha = \frac{\Delta T}{\tau}$$

time between samples of our discrete system

calculated based on desired cutoff frequency

The larger alpha is, the more heavily it weights new information.



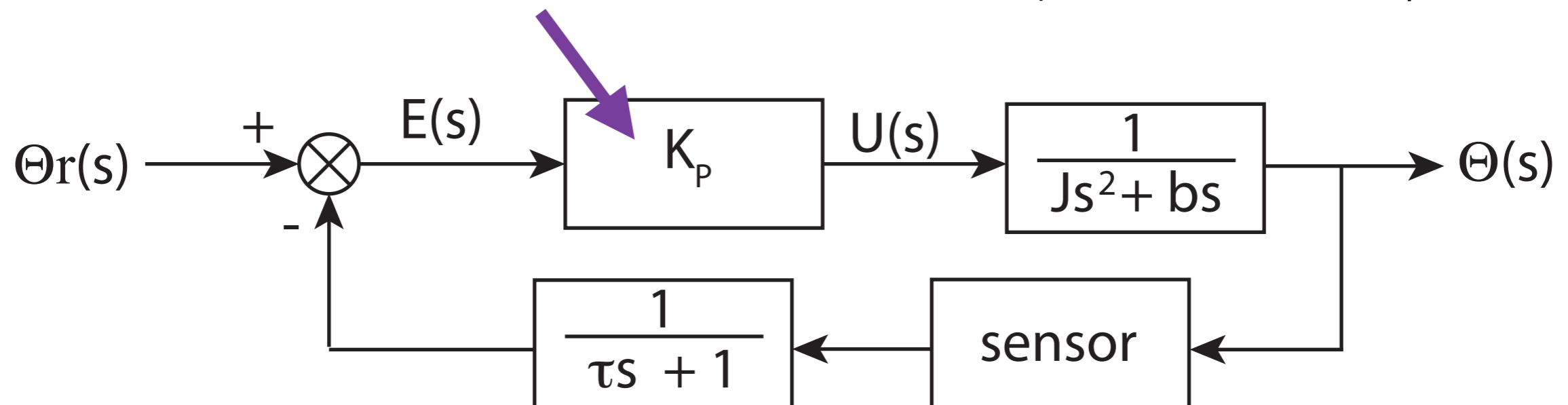
# IIR filter

The filter runs in a loop, such that new measurements are acquired in each time step, and the old measurement will be saved from the previous loop

$$\theta_{updated} = \alpha\theta_{new} + (1 - \alpha)\theta_{old}$$

$$\theta_{old} = \theta_{updated}$$

In the case of a virtual spring with stiffness  $K_p$  and center at  $\theta_r$



# IIR filter derivation

$$H = \frac{1}{\tau s + 1} = \frac{\Theta_{old}}{\Theta_{new}}$$
$$\Theta_{new} = (\tau s + 1)\Theta_{old}$$

Take the inverse Laplace transform...

$$\tau \frac{d\theta_{old}}{dt} + \theta_{old} = \theta_{new}$$

Convert from continuous time to discrete time with timestep  $\Delta T$ ...

$$\tau \frac{\Delta\theta_{old}}{\Delta T} + \theta_{old} = \theta_{new}$$

$$\Delta\theta_{old} = \theta_{updated} - \theta_{old} = \frac{\Delta T}{\tau} (\theta_{new} - \theta_{old})$$

$$\theta_{updated} = \theta_{old} + \frac{\Delta T}{\tau} (\theta_{new} - \theta_{old})$$

$$\theta_{updated} = \frac{\Delta T}{\tau} \theta_{new} + \left(1 - \frac{\Delta T}{\tau}\right) \theta_{old}$$

$$\theta_{updated} = \alpha \theta_{new} + (1 - \alpha) \theta_{old}$$

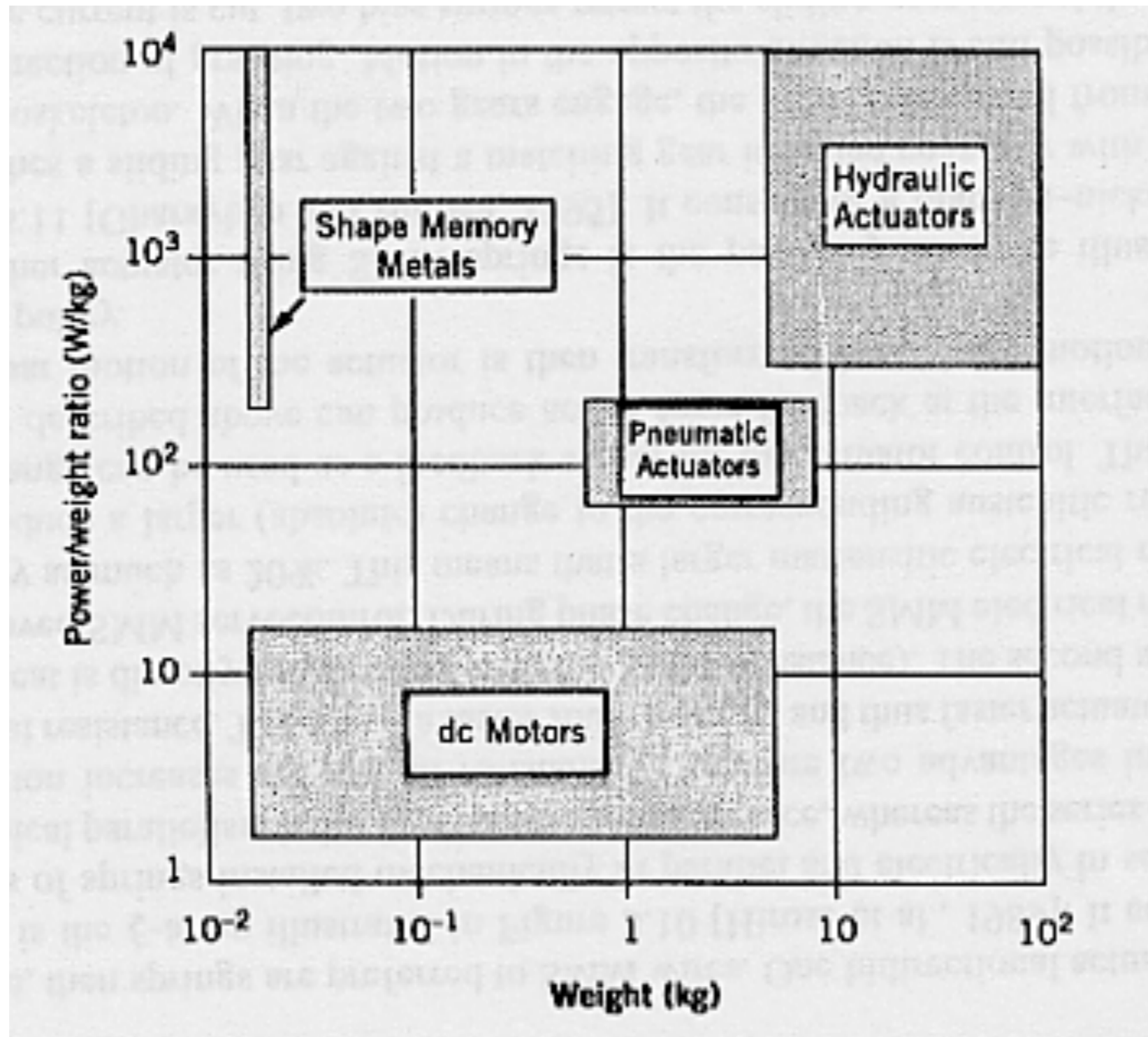
# time-between-ticks

- encoders fare poorly at slow velocities
  - there may be very few ticks during a single servo loop
- instead, some specialized data acquisition boards use a special chip that measures time between ticks
  - fares poorly at high velocities

$$v = \frac{\Delta p}{\Delta t}$$

# actuators

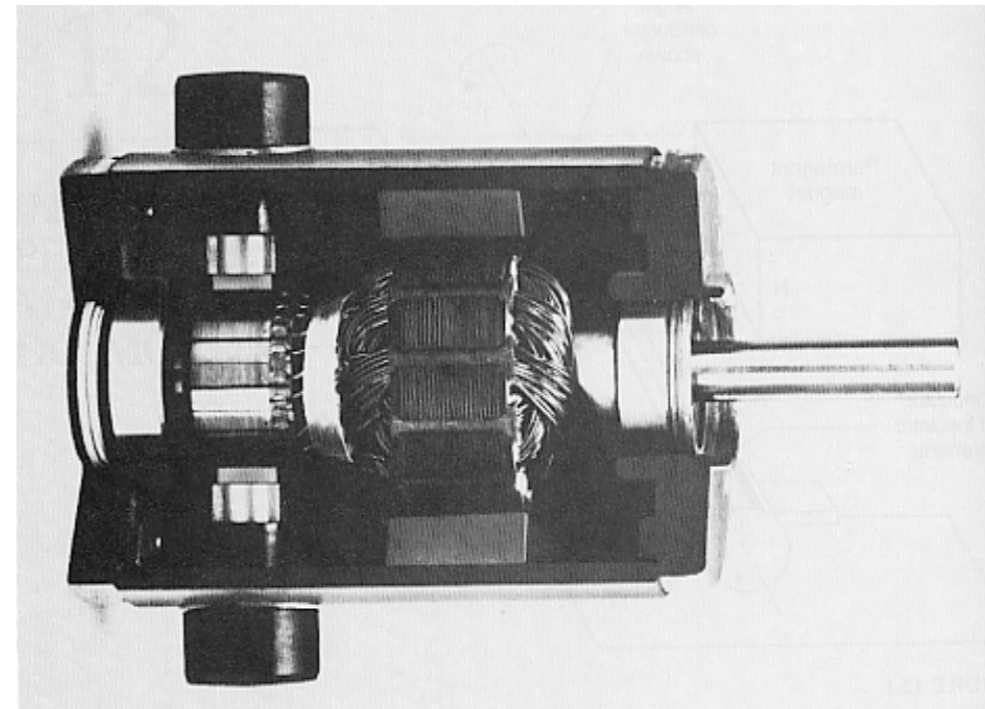
# actuator types



Burdea

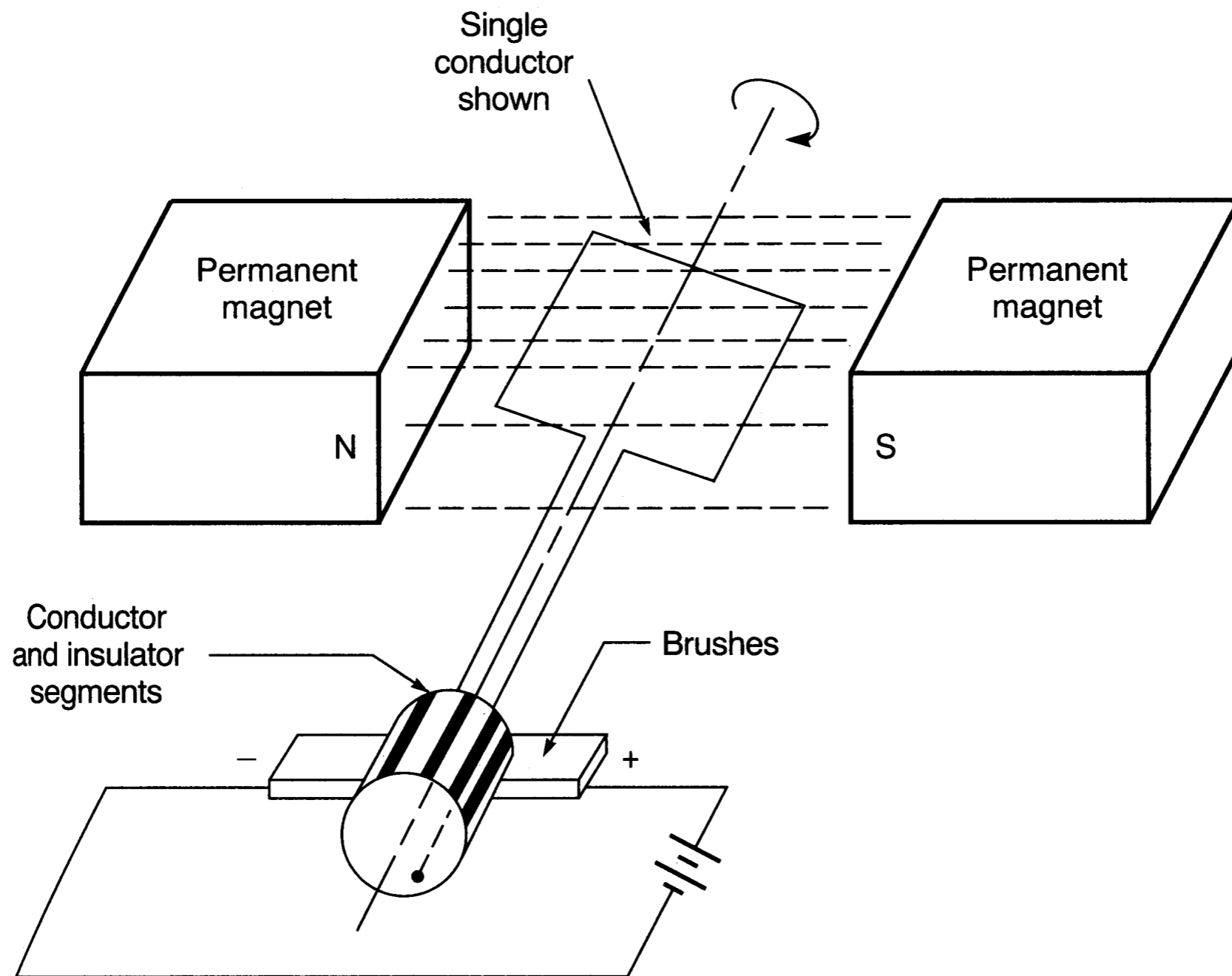
# PM DC brushed motors

- rotating *armature* with coil windings is caused to rotate relative to a permanent magnet



- current is transmitted through brushes to armature, and is constantly switched so that the armature magnetic field remains fixed.

# DC motor components

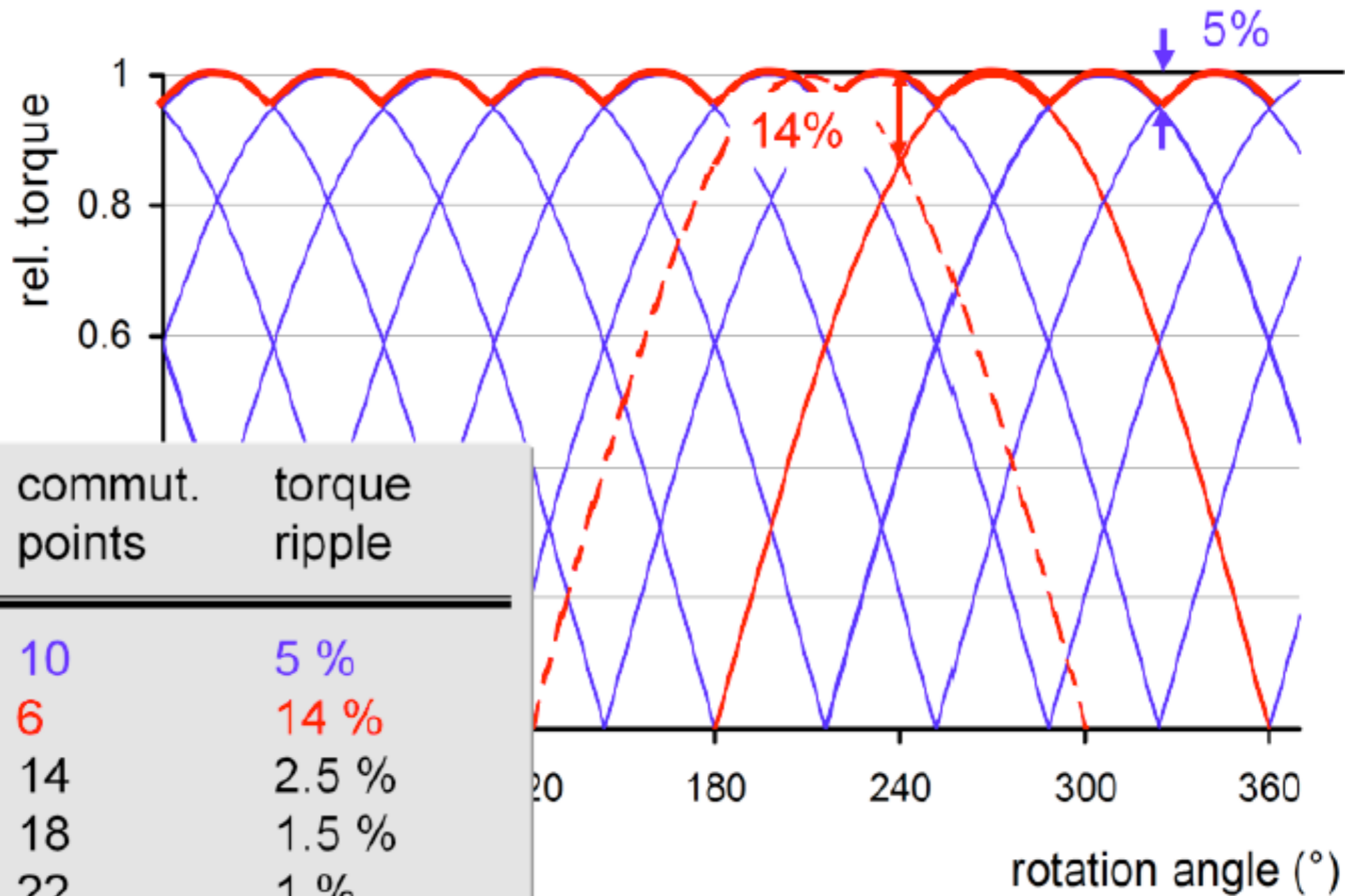


# DC motor terms

- cogging/torque ripple
  - tendency for torque output to ripple as the brushes transfer power
- friction/damping
  - caused by bearings, brushes, and eddy currents
- stall torque
  - max torque delivered by motor when operated continuously without cooling



# torque ripple



commutator segments	commut. points	torque ripple
5	10	5 %
6	6	14 %
7	14	2.5 %
9	18	1.5 %
11	22	1 %
13	26	0.75 %

<http://www.maxonmotorusa.com/>

# motor equations

- torque constant  $k_T$

$$\tau = k_T i$$

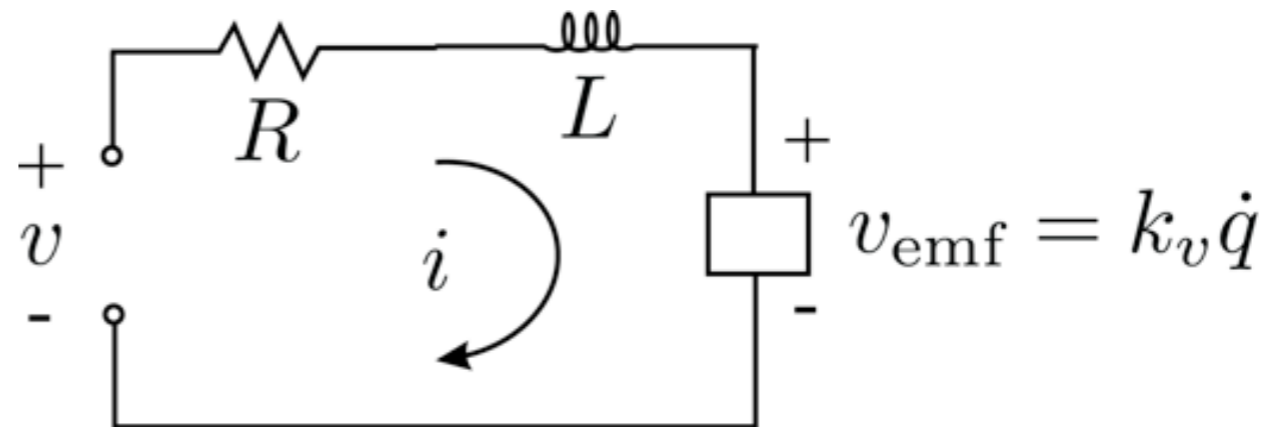
- speed constant  $k_v$

$$v_{\text{emf}} = k_v \dot{q}$$

- dynamic equations

$$v = L \frac{di}{dt} + Ri + v_{\text{emf}}$$

$$m\ddot{q} + b\dot{q} = \tau$$

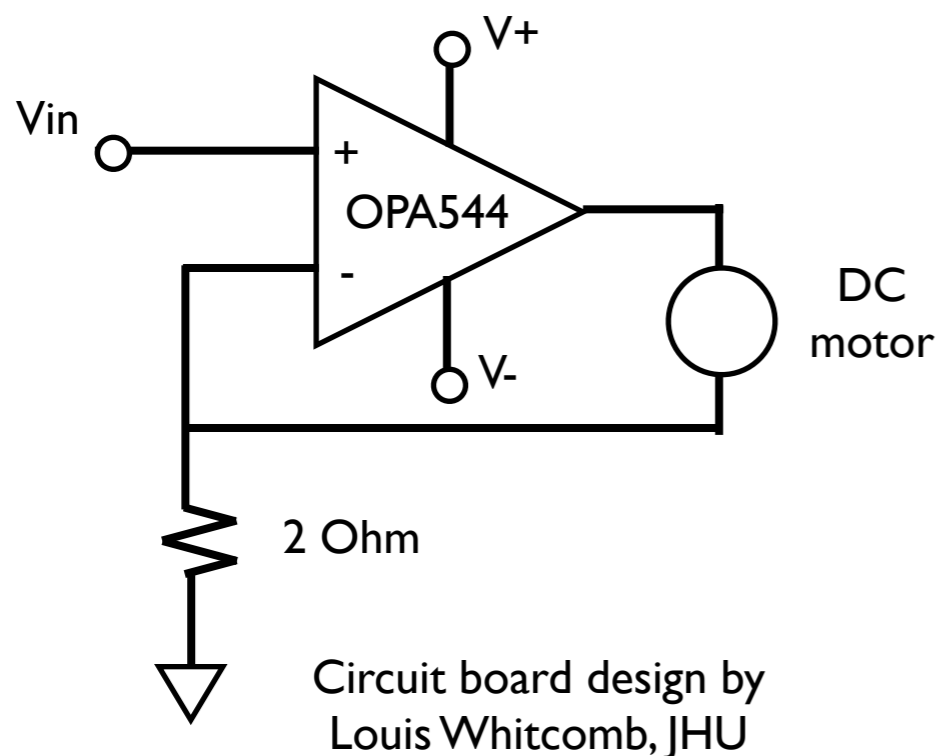


# motor amplifier types

## current amplifier

(voltage controlled current source VCCS)

directly controls current  
current = torque (good!)  
expensive



## voltage amplifier

(voltage controlled voltage source VCVS)

indirectly controls current  
current depends on voltage and state  
often less expensive



ardumotor shield  
<https://www.sparkfun.com/products/9815>  
based on L298 H-bridge

# pulse width modulation



assumes that the average signal is a constant signal



**duty cycle** is the proportion of **on** time to the **period**



<http://www.barrgroup.com/>

useful if you do not have a D/A converter to send analog signals to the motor circuit

switching frequency must be much faster than the mechanical dynamics of the system